# STRUCTURAL ANALYSIS REPORT 95' SELF-SUPPORTING TOWER WEST TISBURY, MASSACHUSETTS 

Prepared for<br>Pyramid Network Services, LLC

SITE: RECC

May 23, 2019


APT Project \#MA2341490

# STRUCTURAL ANALYSIS REPORT 95' SELF-SUPPORTING TOWER DUKES COUNTY, MASSACHUSETTS <br> <br> prepared for <br> <br> prepared for <br> Pyramid Network Services, LLC 

## EXECUTIVE SUMMARY:

All-Points Technology Corporation, P.C. (APT) performed a condition assessment and structural analysis of this 95 ' self-supporting tower. The analysis was performed for Dukes County/Motorola's proposed installation of six omnidirectional whips and two microwave dishes as detailed below. The omnidirectional whips are to be mounted on $6^{\prime}$ sidearms and will be fed by four $1 / 2$ " lines and two $7 / 8$ " lines. The microwave dishes are to be located on leg-mounted pipes and shall be fed by one EW63 line each.

APT's analysis indicates the tower does not meet the requirements of the Massachusetts State Building Code and TIA-222 with the proposed equipment installations. Diagonal bracing and diagonal bolts in one tower section were determined to be inadequately sized. The tower base foundation was also evaluated and determined to be adequately sized under the proposed loading.

## INTRODUCTION:

A condition assessment and structural analysis was performed on the above-mentioned communications tower by APT for Pyramid Network Services, LLC. The tower is located at 9 Flight Path Road in West Tisbury, Massachusetts.

APT visited the tower site on May 1, 2019 to record the existing inventory and assess the condition of the tower. The tower was climbed in its entirety to compile data necessary for performing the structural analysis. The analysis also relied on information provided by others, which included Valmont Structures tower and foundation drawings (drawing \#245211, dated October 15, 2012) and a lease exhibit detailing the proposed equipment changes (dated April 11, 2019).

The structure is a 95 -foot, galvanized steel self-supporting tower manufactured by Valmont Structures. The tower features pipe leg members with angle steel bracing members arranged in an X-braced configuration.

The analysis was performed in accordance with TIA-222-G using the following antenna inventory:

| Antenna | Leg | Elev. | Mount | Coax. |
| :---: | :---: | :---: | :---: | :---: |
| Lightning rod $\mathrm{w} / \mathrm{camera}$ | A | 100' | $10^{\prime} \times 2-3 / 8$ " pipe extension | - |
| 8 " x 6" camera | A | $98^{\prime}$ | On above pipe extension | 1/4" |
| DS1F06F36U-D omnidirectional whip | A | 95 | 6' sidearm | 7/8" |
| (2) 20 ' x 2-1/2" omnidirectional whips | B, C | 85' | (2) 6' x 2-3/8" sidearms w/ $10^{\prime} \times 1-7 / 8^{\prime \prime}$ stabilizers | (2) $1 / 2$ " |
| ANT790F2, ANT150F2 omnidirectional whips | B, C | 80' | (2) $6^{\prime}$ sidearms | (2) $1 / 2$ " |
| 30" high-performance dish, 12 " x 10 " x 3 " panel | A | $\begin{aligned} & 80^{\prime}, \\ & 78^{\prime} \end{aligned}$ | 4' x 4-1/2" pipe on leg | 3/8" |
| 5' x 2-1/2" omnidirectional whip, 8 ' x 3 " omnidirectional whip (inverted) | A | $\begin{aligned} & 76^{\prime}, \\ & 75^{\prime} \end{aligned}$ | 6' x 2-3/8" sidearm w/ 10 ' x 1-7/8" stabilizer | $\begin{aligned} & 7 / 8^{\prime \prime} \\ & 1 / 2 " \end{aligned}$ |
| DS1F06F36U-D omnidirectional whip, SC3-W60A high-performance dish | A | 70' | 6' sidearm, Pipe on leg | $\begin{gathered} \text { 7/8", } \\ \text { EW63 } \end{gathered}$ |
| (2) 20 ' x 2-1/2" omnidirectional whips | B, C | 65 | (2) $6^{\prime} \times 2-3 / 8 "$ sidearms w/ 10' x 1-7/8" stabilizers | 7/8", 1/2" |
| ANT790F2, ANT150F2 omnidirectional whips | A, C | 60' | (2) 6' sidearms | (2) $1 / 2 \times$ |
| SC3-W60A high-performance dish | B | 55' | Pipe on leg | EW63 |
| 20' x 2-1/2" omnidirectional whip | B | 46 ' | $\begin{aligned} & 6^{\prime} \times 2-3 / 8 " \text { sidearm w/ } \\ & 10^{\prime} \times 1-7 / 8^{\prime \prime} \text { stabilizer } \end{aligned}$ | 1/2" |
| Brace for wire feed | A | 12' | 3 ' L1-3/4" x 1/8" angle | N.A. |
| Vacant mount | C | 5 ' | 5 ' x 1" vertical on bracing | N.A. |

## CONDITION ASSESSMENT:

- General Observations: The tower, a 3-legged galvanized steel structure, appeared to be in sound condition. No signs of movement or overstress of the tower were observed. Galvanizing appeared to be in good condition.
- Climbing Facilities: A $3 / 8$ " climber safety cable and climbing pegs are in place on the southeastern leg of the tower.
- Leg Members: Tower legs consist of pipe members, all of which appeared to be in good condition.
- Lattice Bracing: Bracing members are comprised of X-braced angle steel and appeared to be in sound condition. Bracing connections were visually observed to the maximum extent practicable, with no loose or missing bolts observed.
- Splice Connections: Connections were checked by hand for tightness at climbing leg splice locations. No loose or missing splice bolts were observed.
- Antenna Connections: Antenna mounting hardware appeared to be in good condition, with corrosion resistant hardware and galvanized members prevalent.


## STRUCTURAL ANALYSIS:

## Methodology:

The structural analysis was done in accordance with the Massachusetts State Building Code and TIA-222, Revision G (TIA), Structural Standard for Antenna Supporting Structures and Antennas.

The analysis was conducted using a 3-second Ultimate gust wind speed of 155 miles per hour with no ice and $40-\mathrm{mph}$ with $3 / 4$ " radial ice in accordance with the TIA-222-G standard for Dukes County, Massachusetts. The following additional design criteria were used:

| Structure Class: | III |
| :--- | :--- |
| Topographic Category: | 1 |
| Exposure Category: | C |

## Analysis Results:

Analysis of the tower was conducted in accordance with the criteria outlined herein. The following table summarizes the results of the analysis based on stresses of individual leg and bracing members:

| Elevation | Legs | Bracing |
| :---: | :---: | :---: |
| $80^{\prime}-95^{\prime}$ | $15 \%$ | $22 \%$ |
| $60^{\prime}-80^{\prime}$ | $80 \%$ | $61 \%$ |
| $40^{\prime}-60^{\prime}$ | $90 \%$ | $\mathbf{1 2 3 \%}$ |
| $20^{\prime}-40^{\prime}$ | $83 \%$ | $49 \%$ |
| $0^{\prime}-20^{\prime}$ | $97 \%$ | $73 \%$ |

## Bracing, Splice and Anchor Bolts:

Connection bolts were evaluated under the proposed loading. Diagonal bolts were found to be undersized from $40^{\prime}-60^{\prime}$, at a capacity of $141 \%$. All other bolts were found to be adequately sized to support the proposed loading.

## Base Foundation:

Evaluation of the base foundation was performed from original Valmont design drawings. The foundation was determined to be adequately sized under the proposed equipment loading. Factored base reactions imposed with the additional antennas were calculated as follows:

| Reactions | Calculated |
| :---: | :---: |
| Compression (kips) | 167.9 |
| Uplift (kips) | 156.2 |
| Shear (kips) | 14.6 |
| Overturning Moment (ft-kips) | 1281 |

## CONCLUSIONS AND RECOMMENDATIONS:

APT's structural analysis indicates that the 95 -foot self-supporting tower located at 9 Flight Path Road in West Tisbury, Massachusetts does not meet the requirements of the Massachusetts State Building Code and TIA-222 with Dukes County/Motorola's proposed equipment. Diagonal bracing and diagonal bolts in one tower section were determined to require upgrade.

The tower base foundation was also evaluated under the proposed loading and found to be adequately sized.

## LIMITATIONS:

This report is based on the following:

1. Tower is properly installed and maintained.
2. All members are in an undeteriorated condition.
3. All required members are in place.
4. All bolts are in place and are properly tightened.
5. Tower is in plumb condition.
6. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.

All-Points Technology Corporation, P.C. (APT) is not responsible for modifications completed prior to or hereafter which APT is not or was not directly involved. Modifications include but are not limited to:

1. Replacing or strengthening bracing members.
2. Reinforcing vertical members in any manner.
3. Adding or relocating torque arms or guys.
4. Installing antenna mounting gates or side arms.

APT hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon the information contained and set forth herein. If you are aware of any information which is contrary to that which is contained herein, or you are aware of any defects arising from the original design, material, fabrication and erection deficiencies, you should disregard this report and immediately contact APT. APT disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

## Appendix A

Tower Schematic

DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| Generic Lightning Rod 4' copper | 95 | DS1F06F36U-D | 70 |
| 8" fisheye camera | 95 | 6' sidearm | 70 |
| 10'x2 3/8" Pipe Mount | 95 | 4'x4 1/2" Pipe Mount | 70 |
| DS1F06F36U-D | 95 | RFS SC3-W60A HP dish | 70 |
| 6' sidearm | 95 | $10^{\prime} \times 17 / 8^{\prime \prime}$ sidearm stabilizer | 65 |
| 10'x17/8" sidearm stabilizer | 85 | $20^{\prime} \times 2.5$ " omni whip | 65 |
| 20' x 2.5 " omni whip | 85 | 10'x1 7/8" sidearm stabilizer | 65 |
| 6' sidearm | 85 | 6' sidearm | 65 |
| $10^{\prime} \times 17 / 8^{\prime \prime}$ sidearm stabilizer | 85 | $20^{\prime} \times 2.5$ " omni whip | 65 |
| 20' x 2.5 " omni whip | 85 | 6' sidearm | 65 |
| 6' sidearm | 85 | Telewave ANT150F2 | 60 |
| 4'x4 1/2" Pipe Mount | 82-78 | 6' sidearm | 60 |
| Telewave ANT150F2 | 80 | Telewave ANT790F2 | 60 |
| 6' sidearm | 80 | 6' sidearm | 60 |
| Telewave ANT790F2 | 80 | 4'x4 1/2" Pipe Mount | 55 |
| 6' sidearm | 80 | RFS SC3-W60A HP dish | 55 |
| 2.5' HP dish | 80 | 6' sidearm | 46 |
| $12^{\prime \prime} \times 10^{\prime \prime} \times 3$ " panel | 78 | $10^{\prime \prime x} 17 / 8$ " sidearm stabilizer | 46 |
| 5' $\times 2.5$ " omni whip | 76 | 20' x 2" omni whip | 46 |
| 6' sidearm | 76-75 | 3' L1-3/4 $\times 1 / 8$ " angle | 12 |
| $8^{\prime} \times 3^{\prime \prime}$ omni whip | 75 | 5' $\times 1$ ' vertical | 5 |
| $10^{\prime} \times 1$ 7/8" sidearm stabilizer | 75 |  |  |

MATERIAL STRENGTH

| GRADE | Fy |  | Fu |  | GRADE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A572-50 | 50 ksi | 65 ki | Fy | Fu |  |

ALL REACTIONS
ARE FACTORED
MAX. CORNER REACTIONS AT BASE:
DOWN: 167916 lb
SHEAR: 14631 lb
UPLIFT: - 156231 lb
SHEAR: 13738 lb


TORQUE $1406 \mathrm{lb}-\mathrm{ft}$
40 mph WIND - 0.7500 in ICE


TORQUE 6140 lb -ft REACTIONS - 120 mph WIND


## Appendix B

Photographs


Overview photos of 95' self-supporting tower


Photos of existing equipment on tower

Pyramid Network Services
95' Self-Supporting Tower
West Tisbury, Massachusetts


Additional photos of existing equipment and mounts


Photos taken by All-Points Technology Corporation, P.C. on May 1, 2019.


Photos of existing feed lines emerging from pipe conduit



Additional photos of existing feed lines emerging from pipe conduit


Photos of existing feed lines and feed line ladder on tower


Photos of lightning rod and camera (left), and microwave dish with panel (right)


Photo of existing equipment and mounts on tower


Additional photos of existing equipment and mounts



Additional equipment and mount photos


Photo of typical sidearm mount and stabilizer


Photos of typical splice connection


Photo of tower base, including anchor bolts and visible foundation concrete


Photos of typical leg connections to foundation concrete


Photos taken by All-Points Technology Corporation, P.C. on May 1, 2019.


Photos of base of tower leg, and safety climb connection to tower leg


Photos of safety climb and climbing pegs on tower


Photos of ground and surrounding compound from tower


## Appendix C

Calculations

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| :---: | :--- | :--- | :--- |
|  | 9roject | Client | MA2341490 RECC |

## Tower Input Data

The main tower is a $3 x$ free standing tower with an overall height of 95.00 ft above the ground line.
The base of the tower is set at an elevation of 0.00 ft above the ground line.
The face width of the tower is 5.00 ft at the top and 9.00 ft at the base.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
Basic wind speed of 120 mph .
Ultimate wind speed of 155 mph .
Structure Class III.
Exposure Category C.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 0.7500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 40 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in tower member design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Feed Line/Linear Appurtenances

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement <br> ft | Face Offset in | Lateral Offset <br> (Frac FW) | \# | $\begin{gathered} \# \\ \text { Per } \\ \text { Row } \end{gathered}$ | Clear Spacing in | Width or Diameter in | Perimeter <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/4 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 95.00- \\ 10.00 \end{gathered}$ | 0.0000 | -0.08 | 1 | 1 | 0.2500 | 0.2500 |  | 0.05 |
| 1/2 | B | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 85.00- \\ 10.00 \end{gathered}$ | 0.0000 | 0.07 | 1 | 1 | 0.5800 | 0.5800 |  | 0.25 |
| 1/2 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 85.00- \\ 10.00 \end{gathered}$ | 0.0000 | 0.07 | 2 | 2 | 0.5800 | 0.5800 |  | 0.25 |
| 3/8 | B | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 78.00- \\ 10.00 \end{gathered}$ | 0.0000 | -0.03 | 1 | 1 | 0.4400 | 0.4400 |  | 0.08 |
| 7/8 | B | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 75.00- \\ 10.00 \end{gathered}$ | 0.0000 | -0.1 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 1/2 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 75.00- \\ 10.00 \end{gathered}$ | 0.0000 | 0.01 | 1 | 1 | 0.5800 | 0.5800 |  | 0.25 |
| 7/8 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 65.00- \\ 10.00 \end{gathered}$ | 0.0000 | -0.08 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 1/2 | B | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 65.00- \\ 10.00 \end{gathered}$ | 0.0000 | 0.01 | 1 | 1 | 0.5800 | 0.5800 |  | 0.25 |
| 1/2 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 46.00- \\ 10.00 \end{gathered}$ | 0.0000 | 0.01 | 1 | 1 | 0.5800 | 0.5800 |  | 0.25 |
| Feedline <br> Ladder (Af) | B | No | No | $\mathrm{Af}(\mathrm{CaAa})$ | 95.00-6.00 | 0.0000 | 0 | 1 | 1 | 3.0000 | 3.0000 |  | 8.40 |
| 7/8 | C | No | No | Ar (CaAa) | 95.00-8.00 | 0.0000 | -0.08 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 1/2 | C | No | No | Ar (CaAa) | 80.00-8.00 | 0.0000 | -0.01 | 2 | 2 | 0.5800 | 0.5800 |  | 0.25 |
| 7/8 | C | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | 70.00-8.00 | 0.0000 | -0.05 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |


| tnxTOWer | Job | Page |  |
| :---: | :--- | :--- | :--- |
| All-Points Technology <br> 116 Grandview Rd. <br> Conway, NH 03018 <br> Phone: $(603) 496-5853$ <br> FAX: (603) $447-2124$ | Project | Client | MA2341490 RECC |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement <br> ft | Face Offset in | Lateral Offset <br> (Frac FW) | \# | $\begin{gathered} \# \\ \text { Per } \\ \text { Row } \end{gathered}$ | Clear Spacing in | Width or Diameter in | Perimeter <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EW63 | C | No | No | Ar (CaAa) | 70.00-8.00 | 0.0000 | 0.05 | 1 | 1 | 1.5742 | 1.5742 |  | 0.51 |
| 1/2 | C | No | No | Ar (CaAa) | 60.00-8.00 | 0.0000 | 0.01 | 2 | 2 | 0.5800 | 0.5800 |  | 0.25 |
| EW63 | C | No | No | Ar (CaAa) | 55.00-8.00 | 0.0000 | 0.08 | 1 | 1 | 1.5742 | 1.5742 |  | 0.51 |
| Feedline <br> Ladder (Af) | C | No | No | Af (CaAa) | 95.00-6.00 | 0.0000 | 0 | 1 | 1 | 3.0000 | 3.0000 |  | 8.40 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& \begin{tabular}{l}
Placement \\
\(f t\)
\end{tabular} \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight <br>

\hline Generic Lightning Rod 4' copper \& A \& From Leg \& $$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 7.00
\end{aligned}
$$ \& 0.0000 \& 95.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 0.50 \\
& 1.00 \\
& 1.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.50 \\
& 1.00 \\
& 1.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$
\] <br>

\hline 8" fisheye camera \& A \& From Leg \& $$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 3.00
\end{aligned}
$$ \& 0.0000 \& 95.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 0.80 \\
& 0.91 \\
& 1.04
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.53 \\
& 0.63 \\
& 0.73
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 75.00 \\
& 84.24 \\
& 95.48
\end{aligned}
$$
\] <br>

\hline $10^{\prime}$ x2 3/8" Pipe Mount \& A \& None \& \& 0.0000 \& 95.00 \& No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice \& \[
$$
\begin{aligned}
& 2.38 \\
& 3.40 \\
& 4.45
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.38 \\
& 3.40 \\
& 4.45
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 36.50 \\
& 54.35 \\
& 78.71
\end{aligned}
$$
\] <br>

\hline $20^{\prime} \times 2.5$ " omni whip \& B \& From Leg \& \[
$$
\begin{gathered}
6.00 \\
0.00 \\
10.00
\end{gathered}
$$

\] \& 0.0000 \& 85.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 5.00 \\
& 7.03 \\
& 9.07
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.00 \\
& 7.03 \\
& 9.07
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
50.00 \\
86.96 \\
136.55
\end{gathered}
$$
\] <br>

\hline 6 ' sidearm \& B \& None \& \& 0.0000 \& 85.00 \& No Ice 1/2" Ice 1" Ice \& $$
\begin{aligned}
& 4.17 \\
& 6.17 \\
& 8.17
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 2.09 \\
& 3.09 \\
& 4.09
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
75.00 \\
125.00 \\
200.00
\end{gathered}
$$
\] <br>

\hline 10'x1 7/8" sidearm stabilizer \& B \& None \& \& 0.0000 \& 85.00 \& No Ice 1/2" Ice 1" Ice \& $$
\begin{aligned}
& 1.88 \\
& 2.90 \\
& 3.94
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 1.88 \\
& 2.90 \\
& 3.94
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 27.20 \\
& 41.92 \\
& 63.09
\end{aligned}
$$
\] <br>

\hline $20^{\prime} \times 2.5{ }^{\prime \prime}$ omni whip \& C \& From Leg \& \[
$$
\begin{gathered}
6.00 \\
0.00 \\
10.00
\end{gathered}
$$

\] \& 0.0000 \& 85.00 \& No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice \& \[

$$
\begin{aligned}
& 5.00 \\
& 7.03 \\
& 9.07
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.00 \\
& 7.03 \\
& 9.07
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
50.00 \\
86.96 \\
136.55
\end{gathered}
$$
\] <br>

\hline 6 6 sidearm \& C \& None \& \& 0.0000 \& 85.00 \& No Ice 1/2" Ice 1" Ice \& $$
\begin{aligned}
& 4.17 \\
& 6.17 \\
& 8.17
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 2.09 \\
& 3.09 \\
& 4.09
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
75.00 \\
125.00 \\
200.00
\end{gathered}
$$
\] <br>

\hline 10'x1 7/8" sidearm stabilizer \& C \& None \& \& 0.0000 \& 85.00 \& No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice \& \[
$$
\begin{aligned}
& 1.88 \\
& 2.90 \\
& 3.94
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.88 \\
& 2.90 \\
& 3.94
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 27.20 \\
& 41.92 \\
& 63.09
\end{aligned}
$$
\] <br>

\hline $12^{\prime \prime} \times 10^{\prime \prime} \times 3$ " panel \& A \& From Leg \& \[
$$
\begin{aligned}
& 1.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 78.00 \& No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice \& \[

$$
\begin{aligned}
& 1.00 \\
& 1.13 \\
& 1.26
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.32 \\
& 0.40 \\
& 0.49
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 25.00 \\
& 31.87 \\
& 40.56
\end{aligned}
$$
\] <br>

\hline 4'x4 1/2" Pipe Mount \& A \& None \& \& 0.0000 \& 82.00-78.00 \& No Ice 1/2" Ice 1" Ice \& $$
\begin{aligned}
& 1.03 \\
& 1.58 \\
& 1.84
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 1.03 \\
& 1.58 \\
& 1.84
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 43.10 \\
& 56.09 \\
& 72.13
\end{aligned}
$$
\] <br>

\hline 5' x 2.5 " omni whip \& A \& From Leg \& $$
\begin{aligned}
& 6.00 \\
& 0.00 \\
& 2.50
\end{aligned}
$$ \& 0.0000 \& 76.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.53 \\
& 1.84
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.53 \\
& 1.84
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 28.00 \\
& 37.47 \\
& 50.41
\end{aligned}
$$
\] <br>

\hline 8' x 3" omni whip \& A \& From Leg \& $$
\begin{gathered}
6.00 \\
0.00 \\
-4.00
\end{gathered}
$$ \& 0.0000 \& 75.00 \& No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice \& \[

$$
\begin{aligned}
& 2.34 \\
& 3.19 \\
& 3.67
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.34 \\
& 3.19 \\
& 3.67
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 50.00 \\
& 67.51 \\
& 90.37
\end{aligned}
$$
\] <br>

\hline 6' sidearm \& A \& None \& \& 0.0000 \& 76.00-75.00 \& No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice \& \[
$$
\begin{aligned}
& 4.17 \\
& 6.17 \\
& 8.17
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.09 \\
& 3.09 \\
& 4.09
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
75.00 \\
125.00 \\
200.00
\end{gathered}
$$
\] <br>

\hline
\end{tabular}

| tnxTower <br> All-Points Technology <br> 116 Grandview Rd. | Job | 95' Self-Supporting Tower | Page 3 of 6 |
| :---: | :---: | :---: | :---: |
|  | Project | MA2341490 RECC | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 16:00:14 05/23/19 } \end{array}$ |
| Conway, NH 03018 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Client | Pyramid Network Services, LLC | Designed by REA |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight

$l b$ <br>
\hline \multirow[t]{3}{*}{10'x1 7/8" sidearm stabilizer} \& A \& None \& \& 0.0000 \& 75.00 \& No Ice \& 1.88 \& 1.88 \& 27.20 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 2.90 \& 2.90 \& 41.92 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.94 \& 3.94 \& 63.09 <br>
\hline \multirow[t]{3}{*}{$20^{\prime} \times 2.5{ }^{\prime \prime}$ omni whip} \& B \& From Leg \& 6.00 \& 0.0000 \& 65.00 \& No Ice \& 5.00 \& 5.00 \& 50.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.03 \& 7.03 \& 86.96 <br>
\hline \& \& \& 10.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 9.07 \& 9.07 \& 136.55 <br>
\hline \multirow[t]{3}{*}{6 ' sidearm} \& B \& None \& \& 0.0000 \& 65.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>

\hline \& \& \& \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 6.17 \& 3.09 \& \[

125.00
\] <br>

\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{10'x1 7/8" sidearm stabilizer} \& B \& None \& \& 0.0000 \& 65.00 \& No Ice \& 1.88 \& 1.88 \& 27.20 <br>
\hline \& \& \& \& \& \& 1/2' Ice \& 2.90 \& 2.90 \& 41.92 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.94 \& 3.94 \& 63.09 <br>
\hline \multirow[t]{3}{*}{$20^{\prime} \times 2.5$ " omni whip} \& C \& From Leg \& \& 0.0000 \& 65.00 \& No Ice \& 5.00 \& 5.00 \& 50.00 <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice
\] \& 7.03 \& 7.03 \& 86.96 <br>

\hline \& \& \& 10.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 9.07 \& 9.07 \& 136.55 <br>
\hline \multirow[t]{3}{*}{6 ' sidearm} \& C \& None \& \& 0.0000 \& 65.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{10'x1 7/8" sidearm stabilizer} \& C \& None \& \& 0.0000 \& 65.00 \& No Ice \& 1.88 \& 1.88 \& 27.20 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 2.90 \& 2.90 \& 41.92 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 3.94 \& 3.94 \& 63.09 <br>
\hline \multirow[t]{3}{*}{20' x 2" omni whip} \& B \& From Leg \& 6.00 \& 0.0000 \& 46.00 \& No Ice \& 4.00 \& 4.00 \& 45.00 <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 6.03 \& 6.03 \& 75.77 <br>

\hline \& \& \& \& \& \& 1" Ice \& 8.07 \& 8.07 \& 119.12 <br>
\hline \multirow[t]{3}{*}{6 ' sidearm} \& B \& None \& \& 0.0000 \& 46.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{10'x1 7/8" sidearm stabilizer} \& B \& None \& \& 0.0000 \& 46.00 \& No Ice \& 1.88 \& 1.88 \& 27.20 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 2.90 \& 2.90 \& 41.92 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 3.94 \& 3.94 \& 63.09 <br>
\hline \multirow[t]{3}{*}{3 ' L1-3/4 x 1/8" angle} \& A \& None \& \& 0.0000 \& 12.00 \& No Ice \& 0.60 \& 0.03 \& 16.50 <br>

\hline \& \& \& \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 0.81 \& 0.06 \& 22.63 <br>

\hline \& \& \& \& \& \& $$
1^{\prime \prime} \text { Ice }
$$ \& 1.04 \& 0.09 \& 31.54 <br>

\hline \multirow[t]{3}{*}{5' x 1" vertical} \& C \& None \& \& 0.0000 \& 5.00 \& No Ice \& 0.95 \& 0.95 \& 13.60 <br>
\hline \& \& \& \& \& \& 1/2' Ice \& 1.37 \& 1.37 \& 21.14 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 1.68 \& 1.68 \& 32.09 <br>
\hline \multirow[t]{3}{*}{DS1F06F36U-D} \& A \& From Leg \& \& 0.0000 \& 95.00 \& No Ice \& 6.26 \& 6.26 \& 75.00 <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice

\] \& \[

8.79

\] \& \[

8.79

\] \& \[

122.23
\] <br>

\hline \& \& \& $$
11.00
$$ \& \& \& $1{ }^{1 \prime}$ Ice \& 11.03 \& 11.03 \& 183.30 <br>

\hline \multirow[t]{3}{*}{6 ' sidearm} \& A \& None \& \& 0.0000 \& 95.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& 1" Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{Telewave ANT150F2} \& C \& From Leg \& \& 0.0000 \& 80.00 \& No Ice \& 1.29 \& 1.29 \& 15.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.60 \& 1.60 \& 25.28 <br>
\hline \& \& \& 2.50 \& \& \& $1^{\prime \prime}$ Ice \& 1.91 \& 1.91 \& 39.06 <br>
\hline \multirow[t]{3}{*}{6 ' sidearm} \& C \& None \& \& 0.0000 \& 80.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{Telewave ANT790F2} \& B \& From Leg \& 6.00 \& 0.0000 \& 80.00 \& No Ice \& 0.69 \& 0.69 \& 10.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.89 \& 0.89 \& 16.64 <br>
\hline \& \& \& 1.58 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.10 \& 1.10 \& 25.66 <br>
\hline \multirow[t]{3}{*}{6 ' sidearm} \& B \& None \& \& 0.0000 \& 80.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{DS1F06F36U-D} \& A \& From Leg \& 6.00 \& 0.0000 \& 70.00 \& No Ice \& 6.46 \& 6.46 \& 75.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.79 \& 8.79 \& 122.23 <br>
\hline \& \& \& 11.00 \& \& \& 1 " Ice \& 11.03 \& 11.03 \& 183.30 <br>
\hline
\end{tabular}

| tnxTower <br> All-Points Technology <br> 116 Grandview Rd. <br> Conway, NH 03018 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Job | 95' Self-Supporting Tower | Page 4 of 6 |
| :---: | :---: | :---: | :---: |
|  | Project | MA2341490 RECC | Date <br> 16:00:14 05/23/19 |
|  | Client | Pyramid Network Services, LLC | Designed by REA |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$ Side

$$
f t^{2}
$$ \& Weight

$l b$ <br>
\hline \multirow[t]{3}{*}{6 ' sidearm} \& A \& None \& \& 0.0000 \& 70.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{4'x4 1/2" Pipe Mount} \& A \& None \& \& 0.0000 \& 70.00 \& No Ice \& 1.04 \& 1.04 \& 43.10 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 1.58 \& 1.58 \& 56.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.84 \& 1.84 \& 72.13 <br>
\hline \multirow[t]{3}{*}{Telewave ANT150F2} \& C \& From Leg \& 6.00 \& 0.0000 \& 60.00 \& No Ice \& 1.29 \& 1.29 \& 15.00 <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 1.60 \& 1.60 \& 25.28 <br>

\hline \& \& \& 2.50 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.91 \& 1.91 \& 39.06 <br>
\hline \multirow[t]{3}{*}{6' sidearm} \& C \& None \& \& 0.0000 \& 60.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{Telewave ANT790F2} \& A \& From Leg \& 6.00 \& 0.0000 \& 60.00 \& No Ice \& 0.69 \& 0.69 \& 10.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.89 \& 0.89 \& 16.64 <br>
\hline \& \& \& 1.58 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.10 \& 1.10 \& 25.66 <br>
\hline \multirow[t]{3}{*}{6' sidearm} \& A \& None \& \& 0.0000 \& 60.00 \& No Ice \& 4.17 \& 2.09 \& 75.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.17 \& 3.09 \& 125.00 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.17 \& 4.09 \& 200.00 <br>
\hline \multirow[t]{3}{*}{4'x4 1/2' Pipe Mount} \& B \& None \& \& 0.0000 \& 55.00 \& No Ice \& 1.06 \& 1.06 \& 43.10 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 1.58 \& 1.58 \& 56.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.84 \& 1.84 \& 72.13 <br>
\hline
\end{tabular}

## Dishes

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Dish Type | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> ft | Azimuth Adjustment <br> 0 | $3 d B$ <br> Beam <br> Width <br> 0 | Elevation | Outside Diameter <br> ft |  | Aperture Area <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.5' HP dish | A | $\begin{gathered} \text { Paraboloid } \\ \text { w/Shroud (HP) } \end{gathered}$ | From Leg | 1.00 | 0.0000 |  | 80.00 | 2.50 | No Ice | 4.91 | 50.00 |
|  |  |  |  | 0.00 |  |  |  |  | 1/2" Ice | 5.24 | 26.91 |
|  |  |  |  | 0.00 |  |  |  |  | $1{ }^{1 \prime}$ Ice | 5.57 | 38.82 |
| $\begin{aligned} & \text { RFS SC3-W60A HP } \\ & \text { dish } \end{aligned}$ | A | Paraboloid w/Shroud (HP) | From Leg | 1.00 | 0.0000 |  | 70.00 | 3.28 | No Ice | 8.45 | 75.00 |
|  |  |  |  | 0.00 |  |  |  |  | 1/2" Ice | 8.88 | 120.58 |
|  |  |  |  | 0.00 |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 9.32 | 166.17 |
| $\begin{aligned} & \text { RFS SC3-W60A HP } \\ & \text { dish } \end{aligned}$ | B | Paraboloid w/Shroud (HP) | From | 1.00 | 0.0000 |  | 55.00 | 3.28 | No Ice | 8.45 | 75.00 |
|  |  |  | Leg | 0.00 |  |  |  |  | 1/2" Ice | 8.88 | 120.58 |
|  |  |  |  | 0.00 |  |  |  |  | 1 " Ice | 9.32 | 166.17 |


| tnxTOWer | Job | Page |  |
| :---: | :--- | :--- | :--- |
| All-Points Technology <br> 116 Grandview Rd. <br> Conway, NH 03018 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Project | Client | MA2341490 RECC |

## Solution Summary

## Maximum Tower Deflections - Service Wind

| Section No. | Elevation <br> ft | Horz. <br> Deflection in | Gov. Load Comb. | Tilt | Twist 。 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 95-80 | 2.412 | 63 | 0.1981 | 0.0327 |
| T2 | 80-60 | 1.791 | 63 | 0.1932 | 0.0282 |
| T3 | 60-40 | 1.019 | 63 | 0.1563 | 0.0207 |
| T4 | 40-20 | 0.426 | 63 | 0.1006 | 0.0114 |
| T5 | 20-0 | 0.107 | 63 | 0.0472 | 0.0042 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation <br> ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 95.00 | Generic Lightning Rod 4' copper | 63 | 2.412 | 0.1981 | 0.0327 | 306668 |
| 85.00 | $20^{\prime} \times 2.5$ " omni whip | 63 | 1.996 | 0.1965 | 0.0298 | 153334 |
| 82.00 | 4'x4 1/2" Pipe Mount | 63 | 1.873 | 0.1948 | 0.0289 | 116168 |
| 80.00 | 2.5' HP dish | 63 | 1.791 | 0.1932 | 0.0282 | 96298 |
| 78.00 | 12 " x 10" x 3" panel | 63 | 1.709 | 0.1911 | 0.0275 | 78981 |
| 76.00 | 5 ' x 2.5" omni whip | 63 | 1.628 | 0.1886 | 0.0268 | 65424 |
| 75.50 | 6' sidearm | 63 | 1.608 | 0.1879 | 0.0266 | 62626 |
| 75.00 | $8^{\prime} \times 3$ " omni whip | 63 | 1.588 | 0.1872 | 0.0265 | 60044 |
| 70.00 | RFS SC3-W60A HP dish | 63 | 1.391 | 0.1788 | 0.0244 | 42506 |
| 65.00 | $20^{\prime} \times 2.5$ " omni whip | 63 | 1.201 | 0.1683 | 0.0228 | 32897 |
| 60.00 | Telewave ANT150F2 | 63 | 1.019 | 0.1563 | 0.0207 | 26866 |
| 55.00 | RFS SC3-W60A HP dish | 63 | 0.849 | 0.1431 | 0.0183 | 22805 |
| 46.00 | $20^{\prime} \times 2$ " omni whip | 63 | 0.578 | 0.1177 | 0.0142 | 17955 |
| 12.00 | $3^{\prime}$ L1-3/4 x 1/8" angle | 63 | 0.048 | 0.0278 | 0.0023 | 32934 |
| 5.00 | 5 ' x 1" vertical | 63 | 0.017 | 0.0115 | 0.0009 | 79043 |

Bolt Design Data

| Section No. | Elevation <br> $f t$ | Component Type | Bolt Grade | Bolt Size in | Number Of Bolts | Maximum <br> Load per Bolt lb | Allowable <br> Load per Bolt lb | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 95 | Leg | A325N | 0.7500 | 4 | 1841.18 | 29820.60 | $0.062$ | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.7500 | 1 | 1982.13 | 6307.50 |  | 1 | Member Bearing |
|  |  | Top Girt | A325N | 0.7500 | 1 | 173.31 | 6307.50 | 0.027 | 1 | Member Bearing |
| T2 | 80 | Leg | A325N | 0.7500 | 4 | 10361.60 | 29820.60 |  | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.7500 | 1 | 5434.04 | 6307.50 | 0.862 | 1 | Member Bearing |
| T3 | 60 | Leg | A325N | 0.7500 | 6 | 16339.20 | 29820.60 | 0.548 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.7500 | 1 | 8909.87 | 6307.50 | 1.413 | 1 | Member Bearing |
| T4 | 40 | Leg | A325N | 0.7500 | 8 | 16431.70 | 29820.60 | 0.551 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.7500 | 1 | 4215.98 | 9461.25 | 0.446 | 1 | Member Bearing |
| T5 | 20 | Leg | A325N | 0.7500 | 8 | 19054.60 | 29820.60 |  | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.7500 | 1 | 3935.05 | 9461.25 | 0.416 | 1 | Member Bearing |


| tnxTower | Job | 95' Self-Supporting Tower | Page $6 \text { of } 6$ |
| :---: | :---: | :---: | :---: |
| All-Points Technology 116 Grandview Rd. | Project | MA2341490 RECC | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 16:00:14 05/23/19 } \end{array}$ |
| Conway, NH 03018 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Client | Pyramid Network Services, LLC | Designed by REA |

Section Capacity Table

| Section No. | $\begin{aligned} & \text { Elevation } \\ & f t \end{aligned}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} \phi P_{\text {allow }} \\ l b \end{gathered}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 95-80 | Leg | ROHN 2.5 STD | 3 | -8526.53 | 57192.30 | 14.9 | Pass |
|  |  | Diagonal | L2x2x1/8 | 10 | -1950.38 | 8968.45 | 21.7 | Pass |
|  |  |  |  |  |  |  | 31.4 (b) |  |
|  |  | Top Girt | L2x $2 \times 1 / 8$ | 5 | -197.62 | 5299.51 | 3.7 | Pass |
| T2 | 80-60 | Leg | ROHN 2.5 STD | 27 | -45601.50 | 57192.30 | 79.7 | Pass |
|  |  | Diagonal | L2x2x1/8 | 30 | -5504.16 | 8968.45 | 61.4 | Pass |
|  |  |  |  |  |  |  | 86.2 (b) |  |
| T3 | 60-40 | Leg | ROHN 4 STD | 54 | -104269.00 | 116316.00 | 89.6 | Pass |
|  |  | Diagonal | L2x2x1/8 | 58 | -9364.48 | 7617.18 | 122.9 | Fail $\boldsymbol{X}$ |
|  |  |  |  |  |  |  | 141.3 (b) |  |
| T4 | 40-20 | Leg | ROHN 5 STD | 75 | -140093.00 | 169372.00 | 82.7 | Pass |
|  |  | Diagonal | L2x2x3/16 | 79 | -4013.34 | 8147.41 | 49.3 | Pass |
| T5 | 20-0 | Leg | ROHN 5 STD | 96 | -163401.00 | 169372.00 | 96.5 | Pass |
|  |  | Diagonal | L2x2x3/16 | 100 | -4394.84 | 6003.06 | 73.2 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T5) | 96.5 | Pass |
|  |  |  |  |  |  | Diagonal (T3) | 141.3 | Fail $\boldsymbol{X}$ |
|  |  |  |  |  |  | Top Girt (T1) | 3.7 | Pass |
|  |  |  |  |  |  | Bolt Checks | 141.3 | Fail $\boldsymbol{X}$ |
|  |  |  |  |  |  | RATING = | 141.3 | Fail $X$ |

## All-Points Technology Corp., P.C.

116 Grandview Road
Conway, NH 03818
(603) 496-5853

Client:
Pyramid Network Services, LLC
Site: RECC
Job:
West Tisbury, MA
Job No.: MA2341490
Calculated By:
R. Adair

Date: 23-May-19

## Program assumes:

Mat is square in plan view.
Water table is below bottom of mat.
Unit weight of concrete $=\quad 150 \mathrm{pcf}$
Unit weight of soil = 100 pcf
Self-supporting tower with 3 piers
Information to be provided:
Pier is round or square in plan dimension ("R" or "S")
OTM = Overturning Moment to be resisted
$\mathrm{H}=$ Height from ground surface to top of mat (if buried)

| Shape $=$ | R |  |
| ---: | :--- | ---: |
| OTM | $=$ | 1281 ft -kips |
| $\mathrm{H}=$ | $3.0 \mathrm{ft}$. |  |
| $\mathrm{P}_{\mathrm{M}}=$ | $3.5 \mathrm{ft}$. |  |
| $\mathrm{y}=$ | $1.50 \mathrm{ft}$. |  |
| $\mathrm{X}=$ | $18.00 \mathrm{ft}$. |  |
| $\mathrm{~d}=$ | 2.5 ft. |  |
| $\mathrm{S}=$ | 7 |  |

$\mathrm{P}_{\mathrm{M}}=$ Projection of pier above mat
$\mathrm{P}_{\mathrm{M}}=3.5 \mathrm{ft}$.
$\mathrm{y}=$ Thickness of mat
$\mathrm{x}=$ Width of mat
d = Diameter of round pier
$\mathrm{d}=$
2.5 ft .

S = Size of tension bars
S
Mass of tower and appurtenances (below)
Results:

| Component | Mass | Moment Arm | Moment Resist. |
| ---: | ---: | ---: | ---: |
| Pier | 2.6 kips | $9 \mathrm{ft}$. | 23.2 ft -kips |
| Overburden | 116.2 kips | 9 ft | 1046.0 ft -kips |
| Mat | 72.9 kips | 9 ft. | 656.1 ft -kips |

Overturning Moment Resistance $=1725.27 \mathrm{ft}$-kips
Factor of Safety $=\quad 1.35 \quad$ SATISFACTORY
Concrete Quantity $=\quad 19.9$ c.y.

